

# Membrane Wing Aerodynamics for $\mu$ AV Applications

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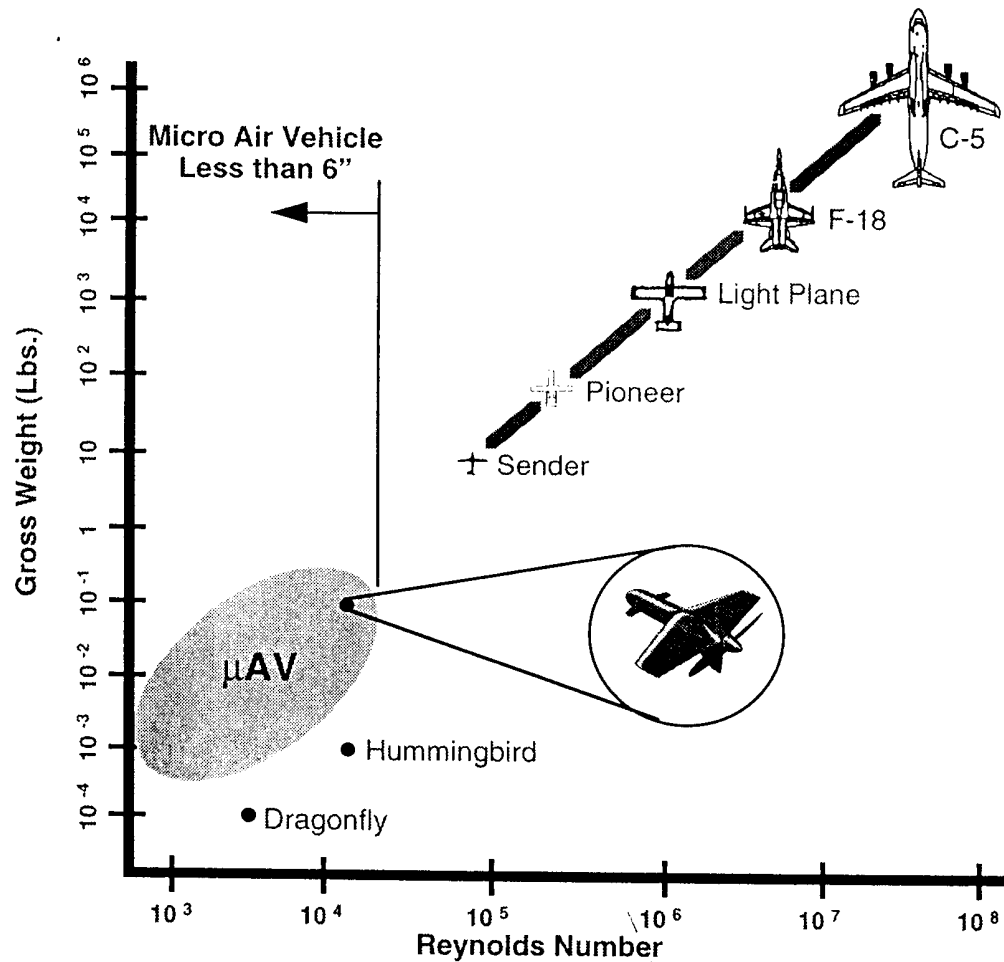
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# Scope of This Talk

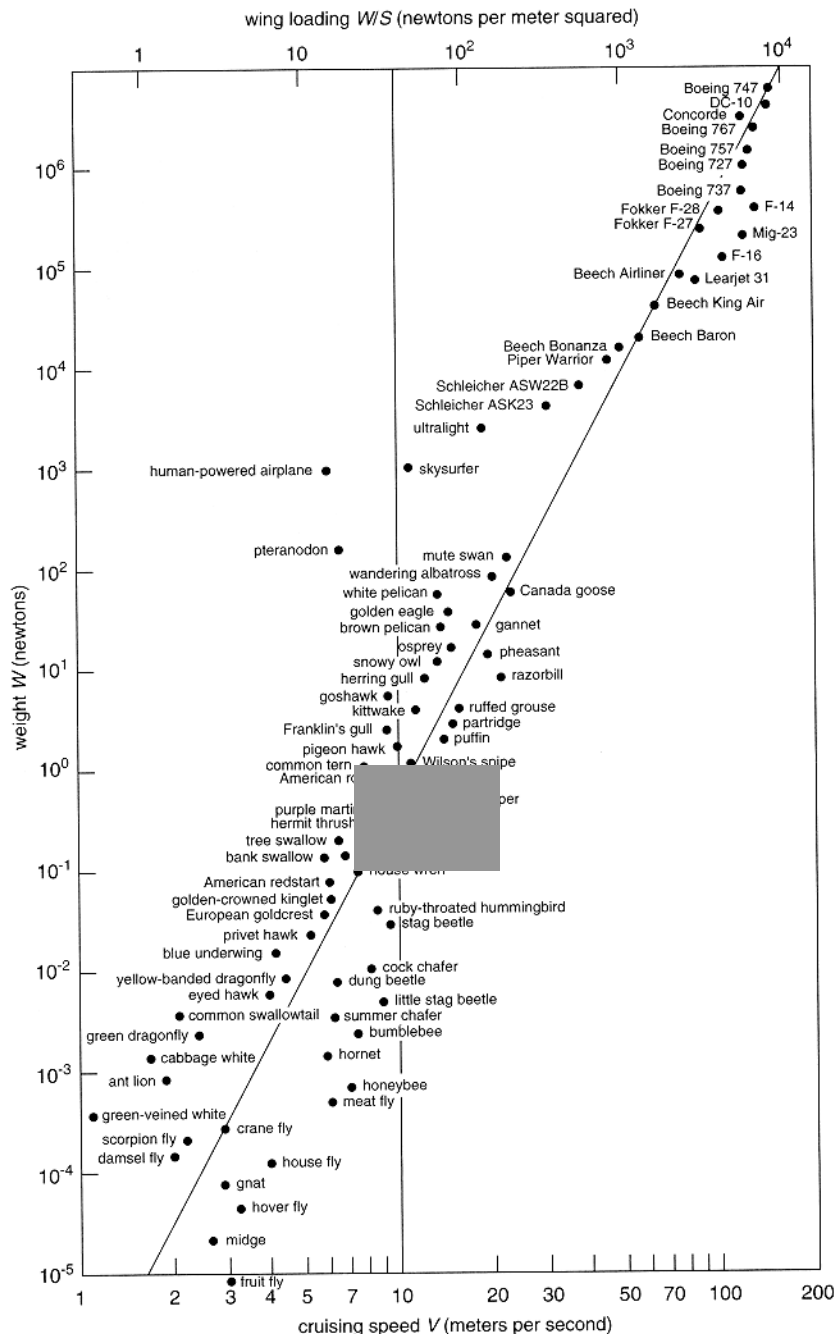
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- Overview of Univ. Florida  $\mu$ AV
- Summarize computational capabilities for fluid/structure interactions: membrane and surrounding viscous flow.
- Present the aerodynamics of self-excited membrane and MAV implications.
- Discuss the wing shape optimization for  $\mu$ AV Applications.

# Characteristics of $\mu$ AV



- Micro Air Vehicle ( $\mu$ AV) smaller than 6", Speed 10m/s. Many applications.
- Low Reynolds number ( $10^4$ - $10^5$ ) condition: degraded L/D
- Flight environment intrinsically unsteady.



## The Great Flight Diagram

(modified from Tennekes)

weight  $\sim l^3$

wing loading  $\sim l$

wing beat freq.  $\sim l^{-1}$

stall speed  $\sim (2W/rSC_l)$   
 $\sim l^{0.5}$

$P/W = (D/L)V \sim l^{0.5}$

*Small Birds:*

*Can fly slower,*

*Need to flap faster,*

*Need less energy density,*

*But can store MUCH less,*

*Can sustain*

*higher impact velocity.*

# **μAV: Geometric & Aerodynamic Scaling**

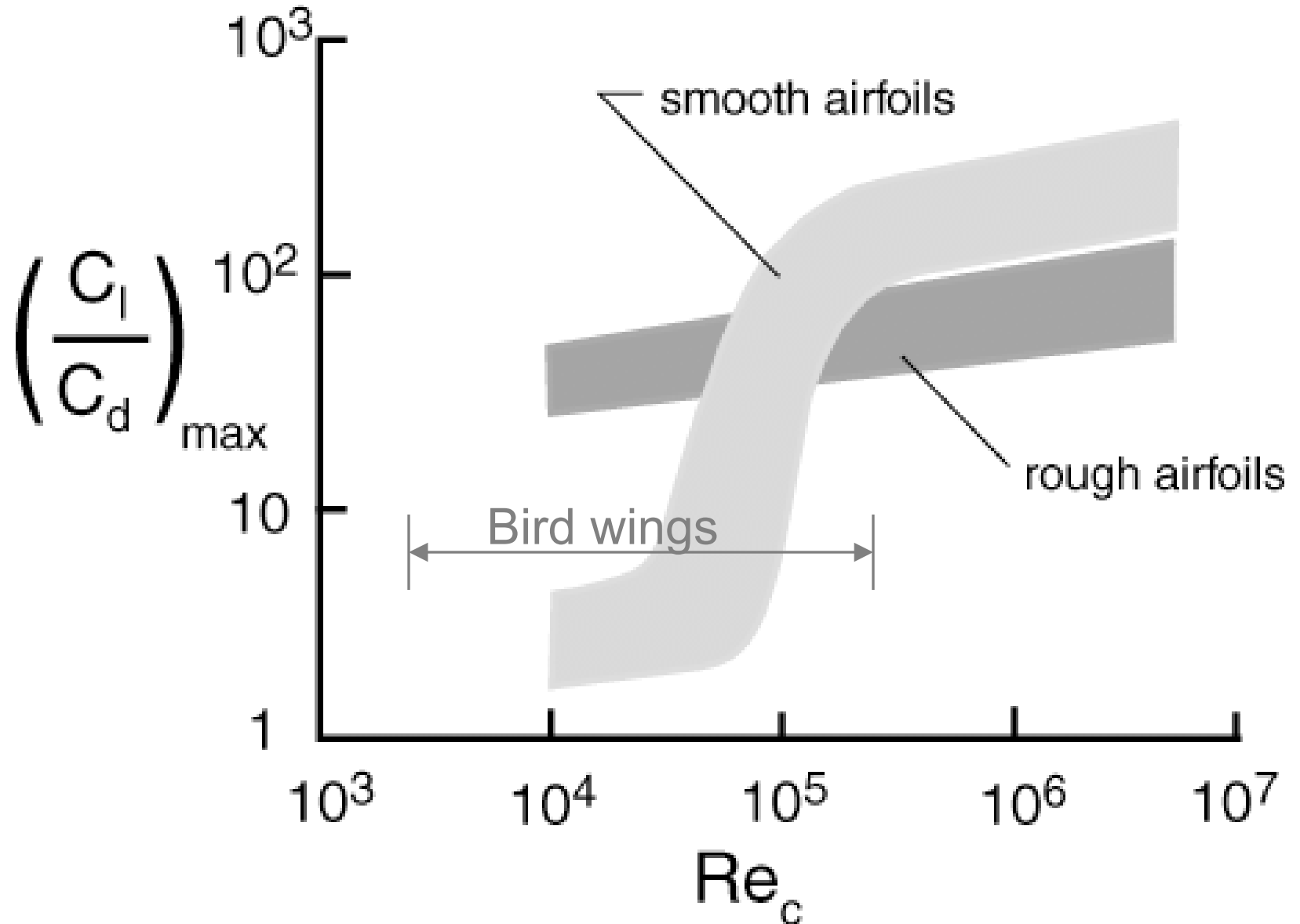
**Geometric Scaling:** If aerodynamics is unchanged, the power requirement decreases as the vehicle size is reduced.

**Aerodynamic Scaling:** Aerodynamic performance degrades as the vehicle size, and hence Re, decreases.

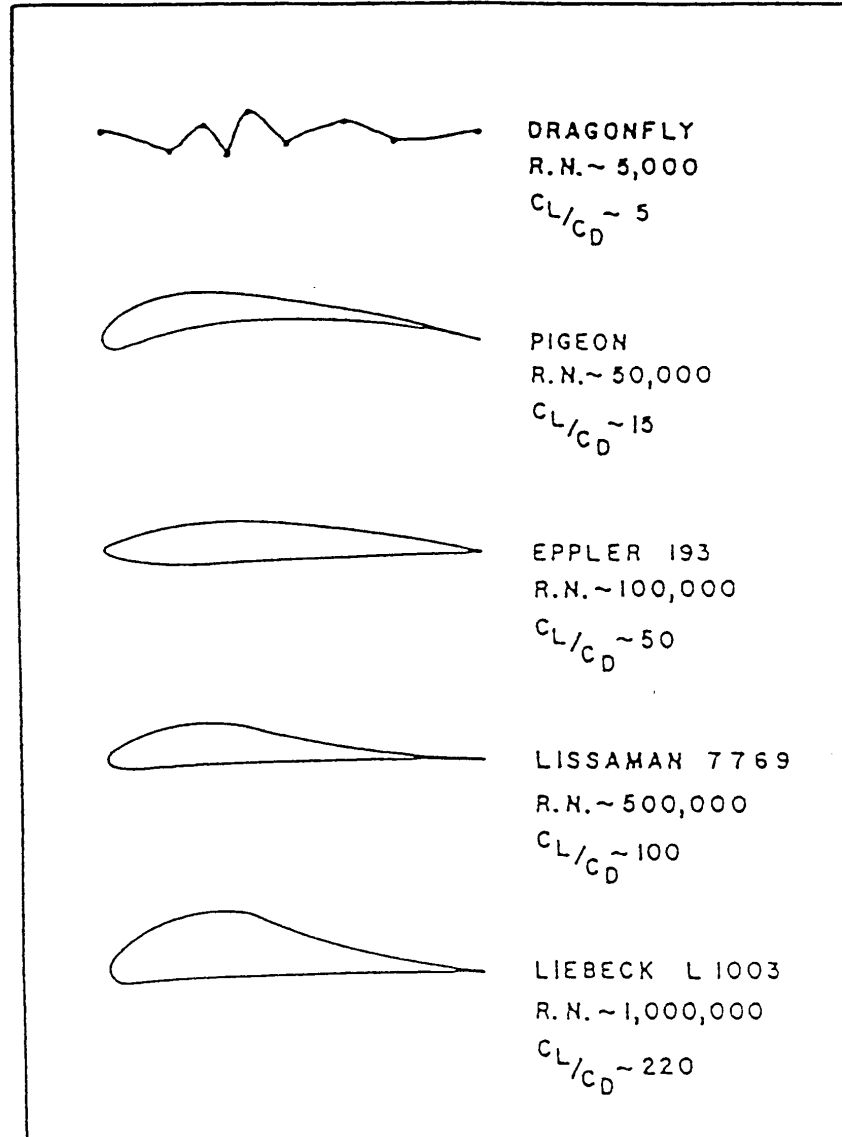
$$P=W\left(\frac{C_D}{C_L^{3/2}}\right)\sqrt{\left(\frac{2}{\rho}\right)\left(\frac{W}{S}\right)}$$

# Low Reynolds Number Airfoils

- Gusts affect small birds and  $\mu$ AVs more than large ones

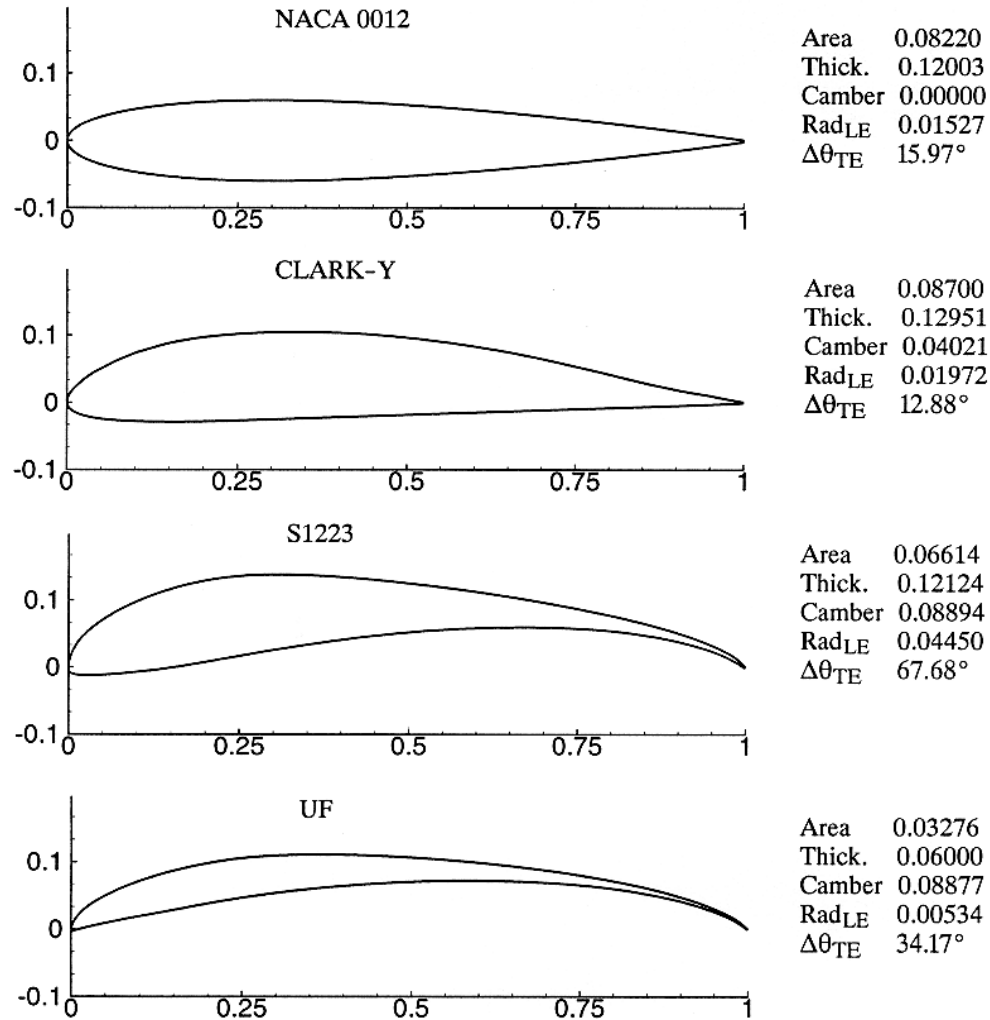


# Representative Low-Reynolds-Number Airfoils (from Lissaman)

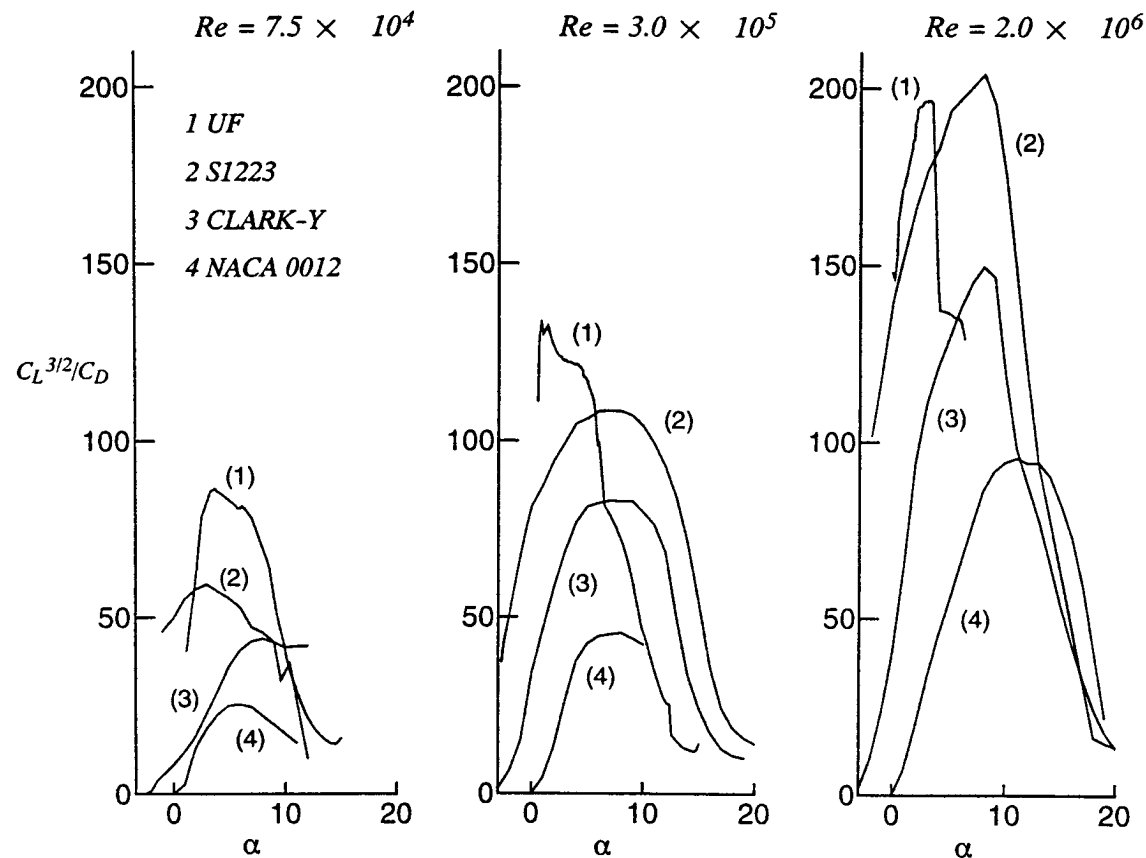




# Selected Airfoil Profiles



# Effects of Re, Airfoil Shape, and AoA on Power Index

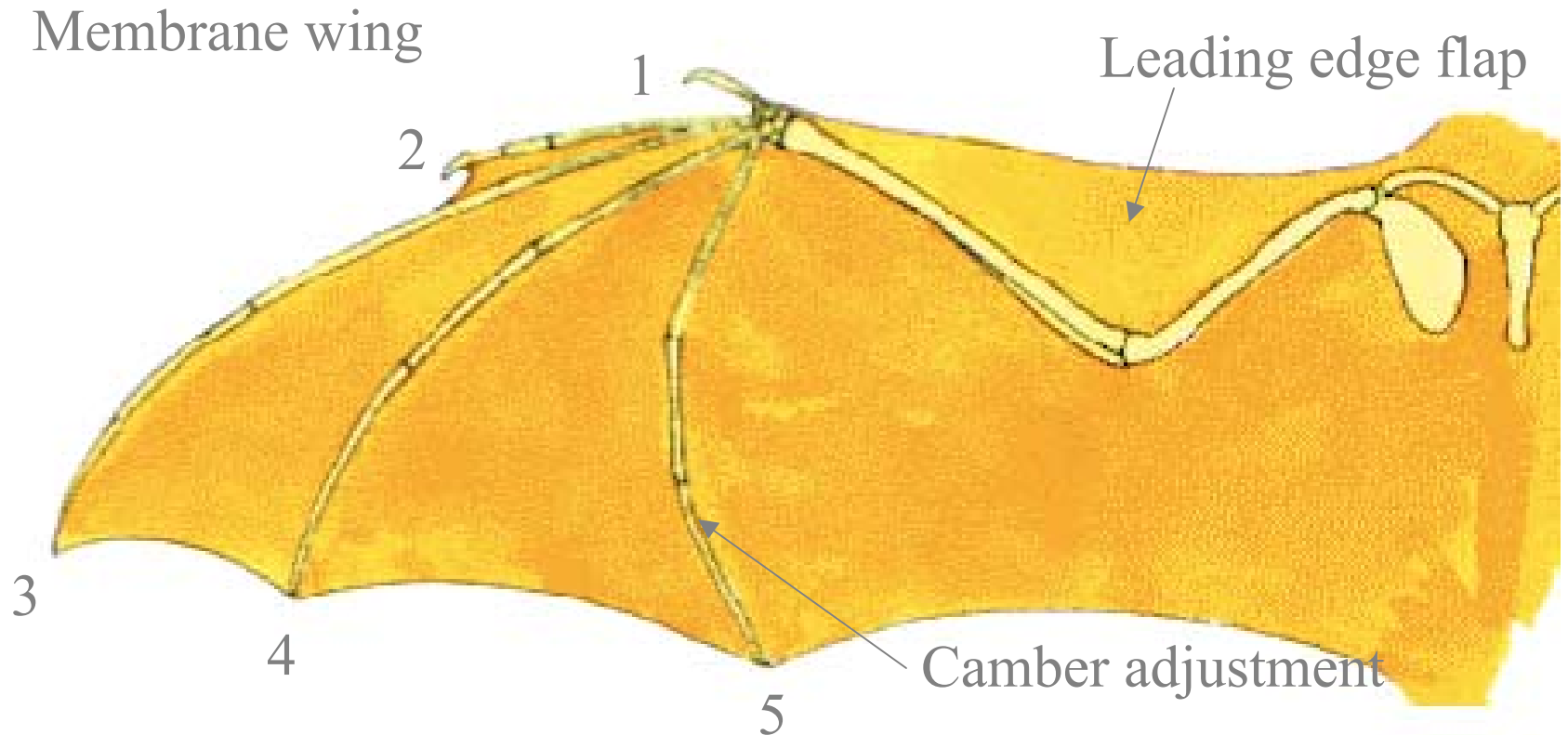


# Membrane-Based $\mu$ AV Concept at U. Florida

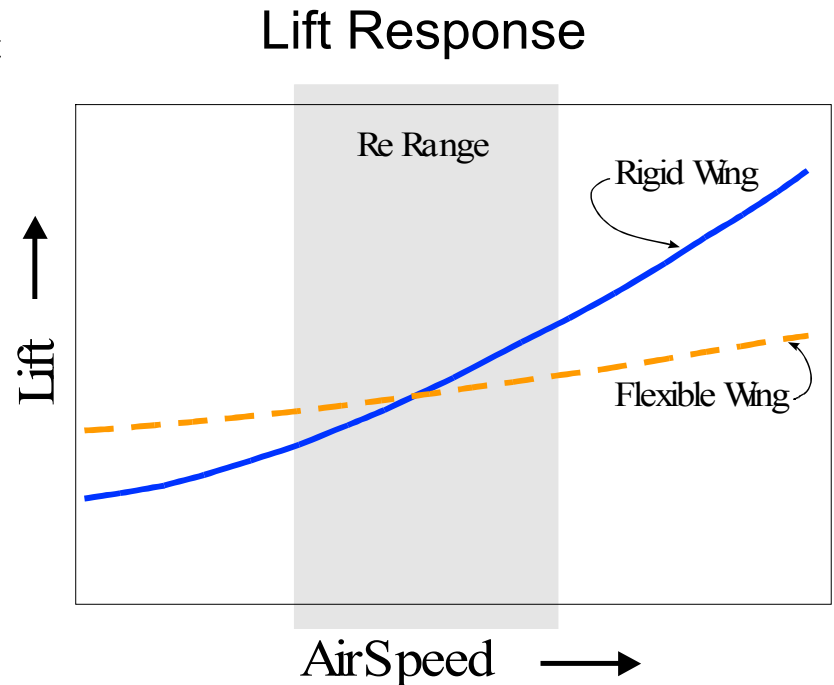
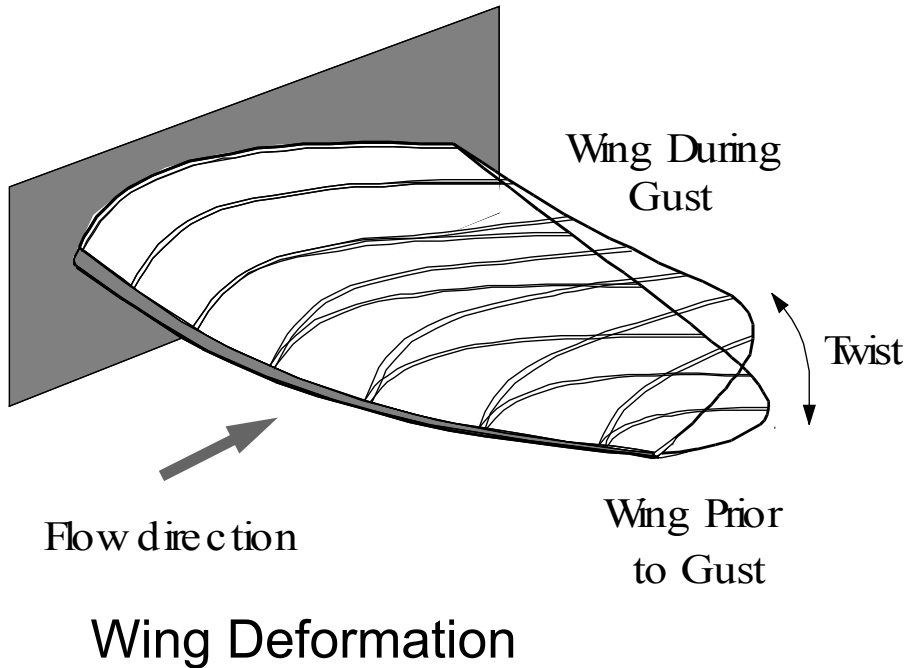


- Wingspan: 6 inches
- Length: 5.5 inches
- Weight w/payload, video camera: 2 ounces
- Range: 0.5 mile with off the shelf components
- Endurance: 10 minutes
- Speed Range: 10 – 35 miles/hour
- Propulsion: electric motor
- Batteries: rechargeable Lithium polymer
- Altitude: up to 500 feet AGL

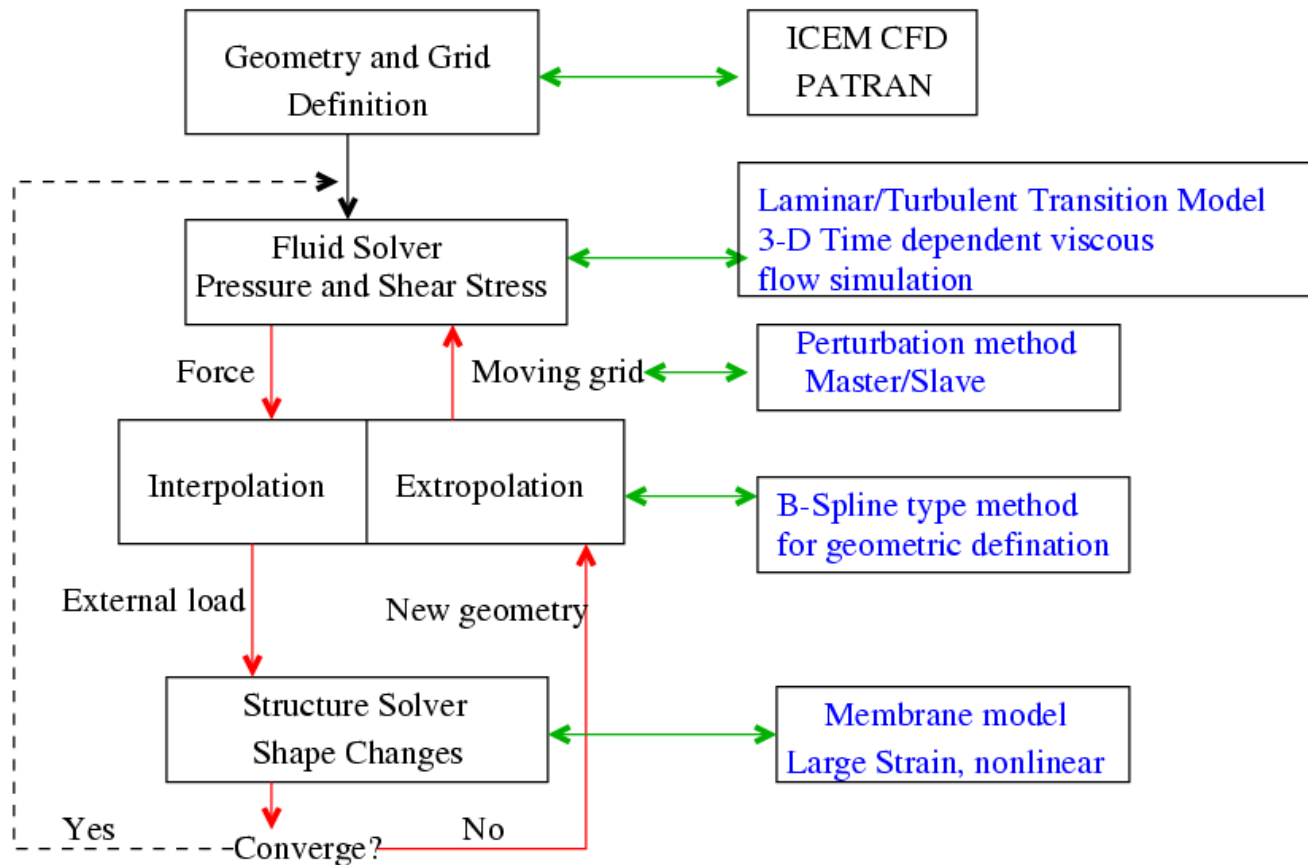
# Bat Wing Morphology



# Adaptive Washout for Gust Suppression



# Computational Fluid/Structure Interaction



- **Fluid solver:** Calculate the external force.
- **Structure solver:** Calculate the shape change.
- **Moving boundary:** Regenerate the CFD grid
- **Interface:** Exchange information between fluid and structure solvers.

# Approach

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## ➤ Structure model

- Dynamic membrane model with finite element.
- Expect substantial deformation: nonlinearity.

## ➤ Fluid flow solver

- A pressure-based method for 3-D full Navier-Stokes equations

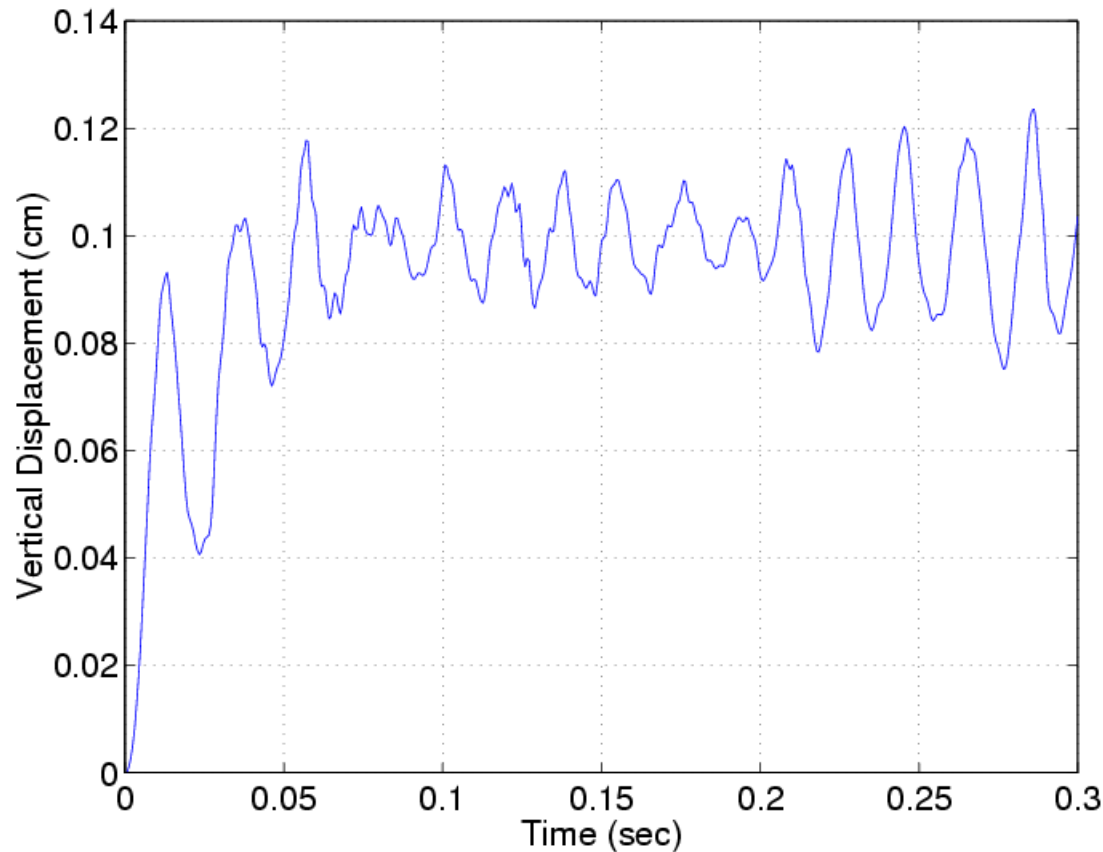
## ➤ Grid regeneration

- 3-stage algebraic TFI-like method.

## ➤ Interpolation

- Thin Plate Spline (TPS) interpolation method

# Displacement of trailing edge at mid-span



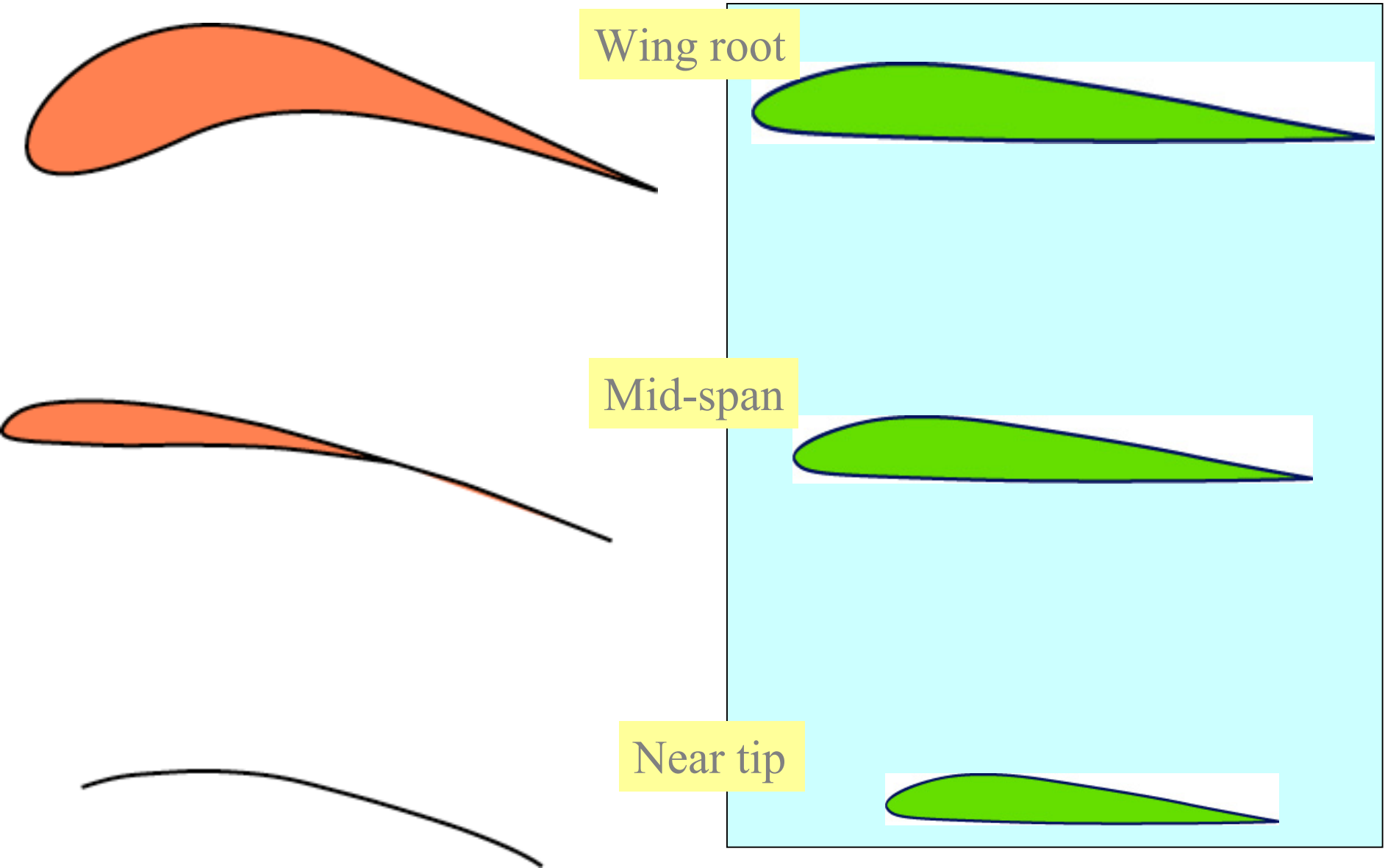
- Steady Free Stream,  $Re = 9 \times 10^4$ ,  $AoA = 6^\circ$
- Periodic oscillation of the trailing edge point.
- Frequency = 67 Hz. (Typical wind gust: 1 Hz)
- The effective angle of attack reduced.



# Wing Cross Section: Optimization?

Pigeon wing

Conventional Wing



# Optimization Scope and Approach

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Minimize  $C_D / C_L$

Subject to

$$1: C_L \geq C_{L\text{baseline}}$$

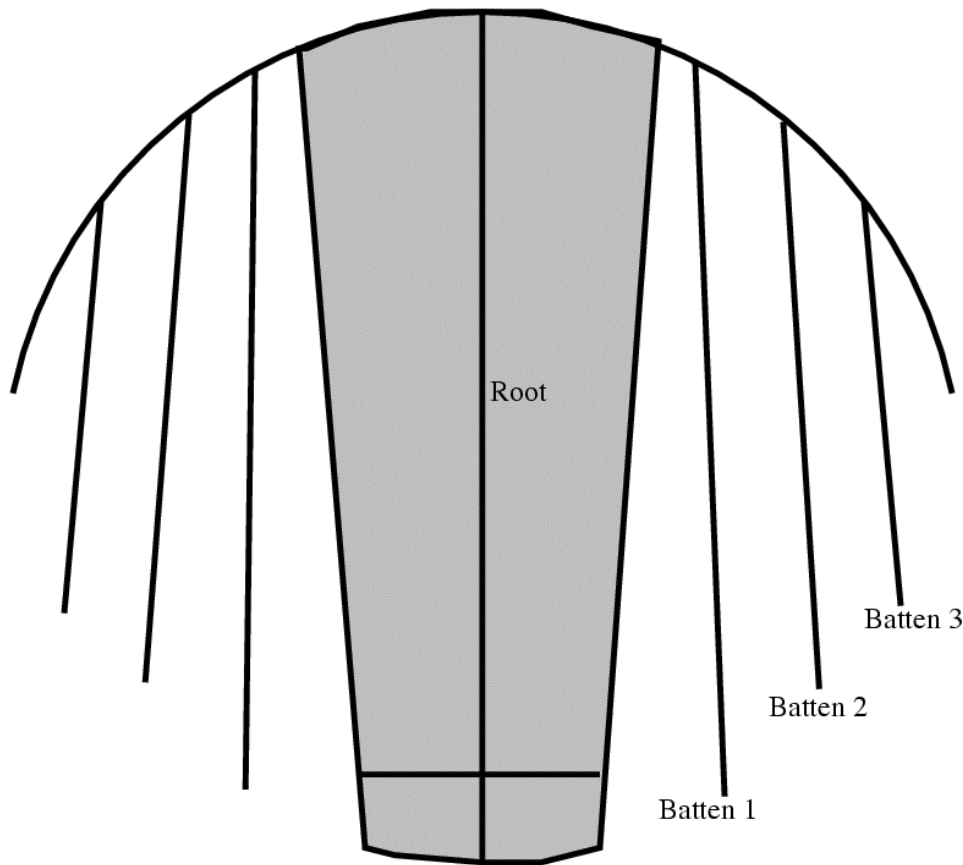
$$2: \text{Convexity constraint: } Y_1 \geq \frac{Y_2 + y_2 - Y_0}{x_2 - x_0}(x_1 - x_0) + y_0 - y_1 + \varepsilon$$

$$3: Y_i^L \leq Y_i \leq Y_i^U, \quad i = 1, N$$

- Maximize L/D; Maintain lift; Keep cross-section convex.
- A direct optimization of membrane wing is time-demanding: Optimize the rigid wing as a surrogate.
- Design Optimization Tools (DOT) used as the optimizer.
- An automatic grid regeneration tool is used to regenerate the CFD grid as each analysis.

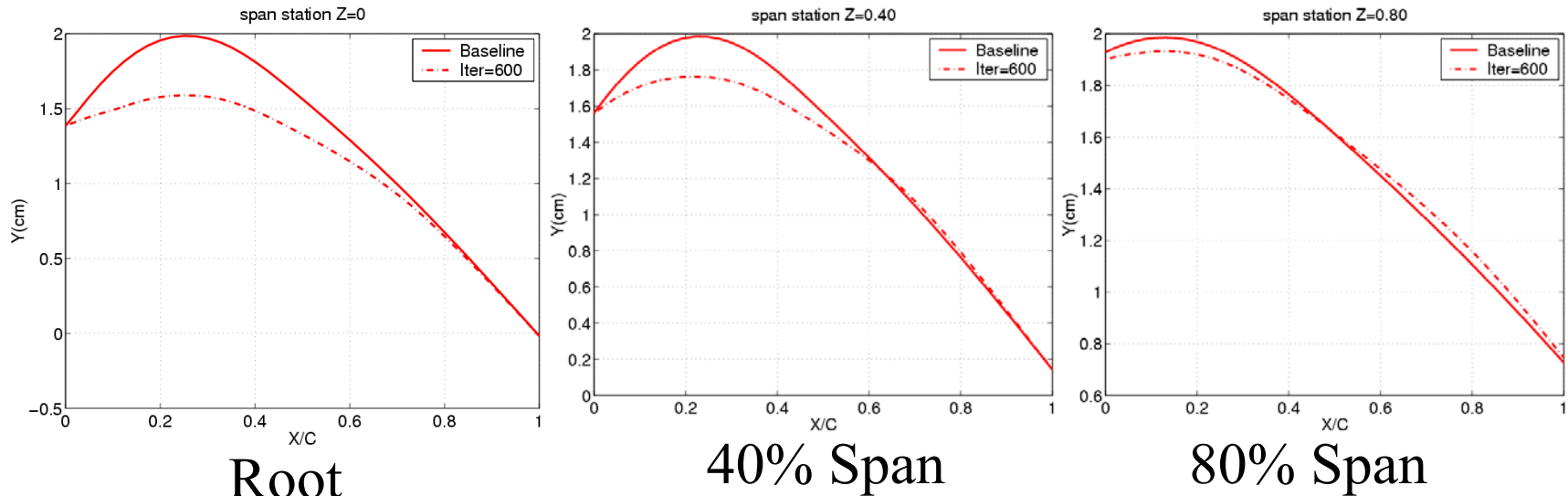


# Choice of Design Variables



- The baseline design is based results from Xfoil (Drela): which uses a two-equation boundary layer integral formulation & inviscid-BL coupling.
- 6 Design Variables: Three each on battens1 and 2.

# Airfoil Shapes in Spanwise Direction



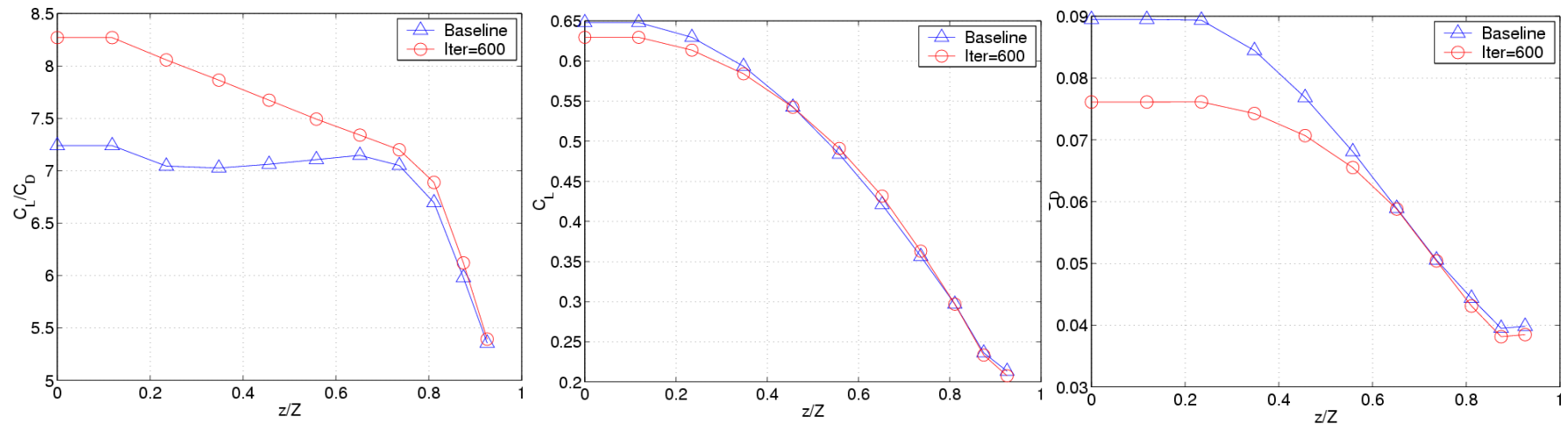
➤ Compared to the baseline, camber decreases near the root while increases near the tip.

➤ Overall, the camber is still higher at the root (4.8%) than at the tip (4%).

➤ In optimization we maintain angle of attack at  $6^\circ$ .

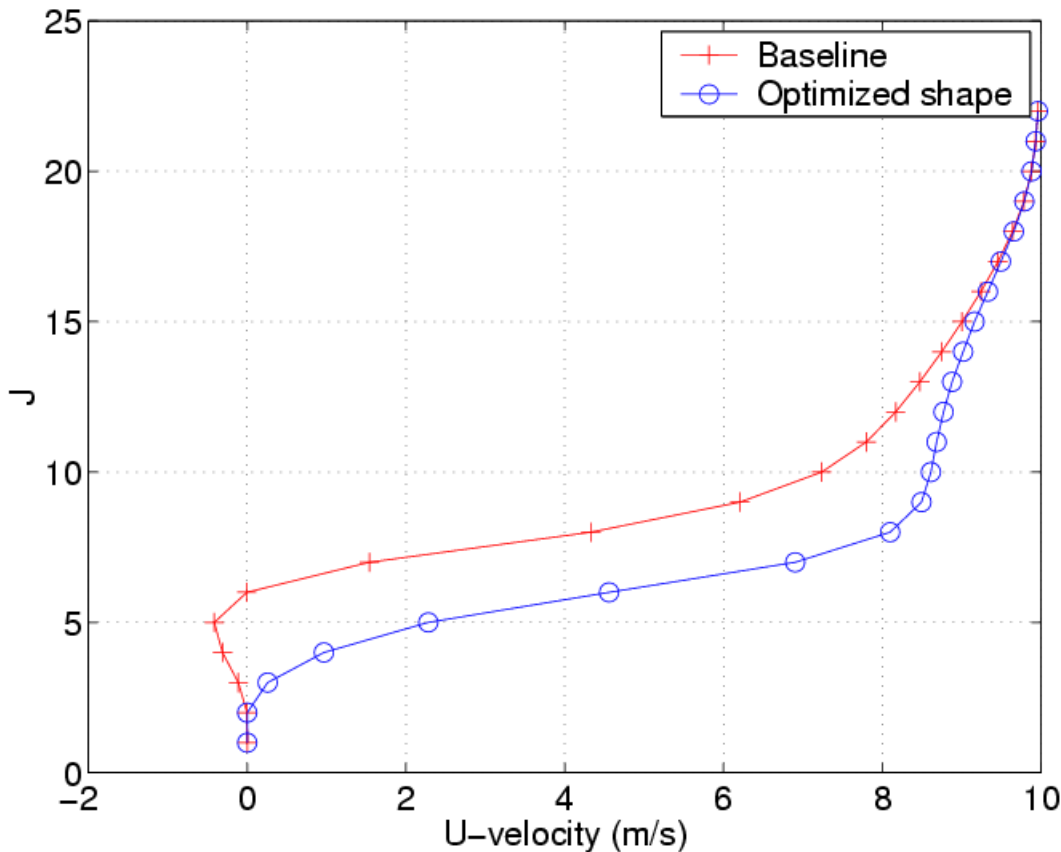


# Spanwise Aerodynamics at Design Point: Rigid Wing at $\text{AoA}=6^\circ$



- Optimization can improve  $L/D$ .
- The improvement is largely located within 70% of the inner wing.
- Lift coefficient maintains the same even though camber reduces.
- The improvement is largely due to lower form drag.

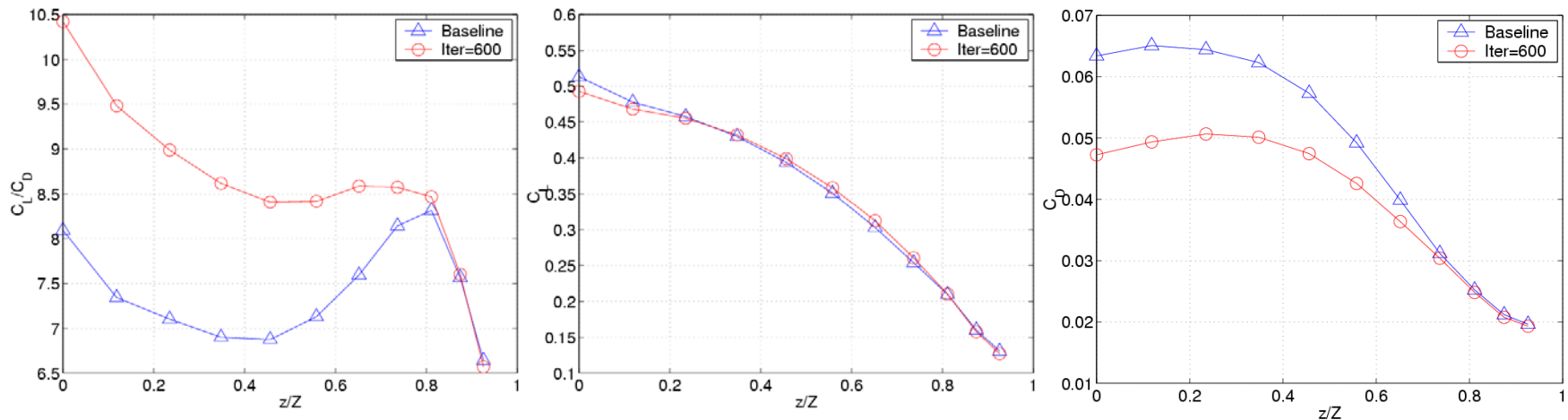
# Velocity Profile Near Root: Rigid Wing



➤  $AoA=6^\circ$

➤ The optimized wing suppresses the flow separation.

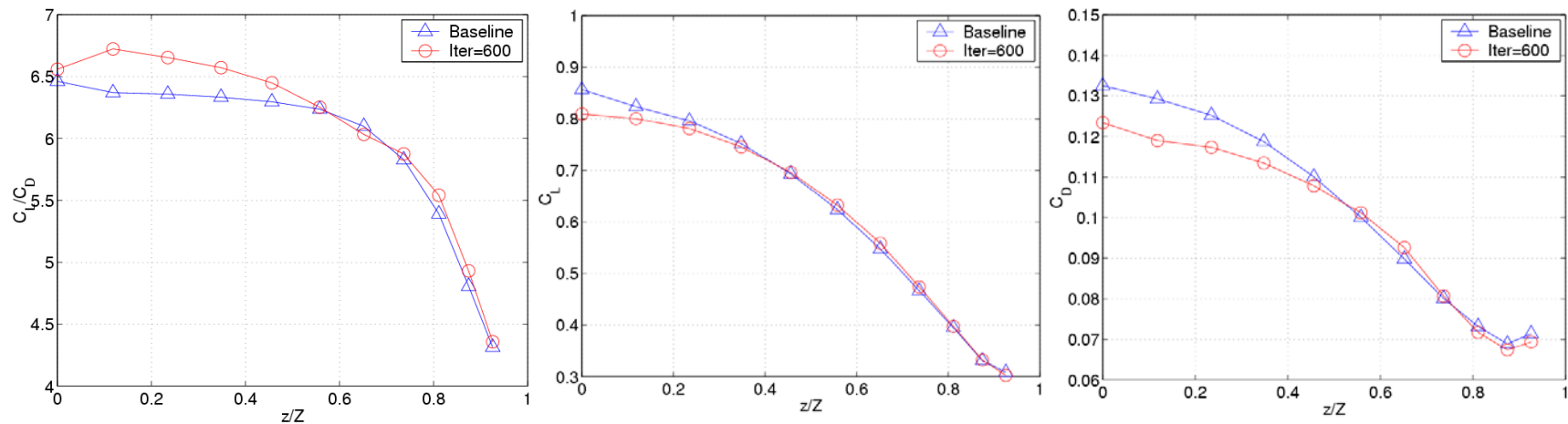
# Spanwise Aerodynamics at Off-Design Point: Rigid Wing at $AoA=3^\circ$



➤ The improvement is substantial at low  $AoA$ , and consistent with the design point, is largely located within 70% of the inner wing.

➤ Same as the design point, the lift maintains the same even though camber reduces, and the improvement is largely due to lower form drag.

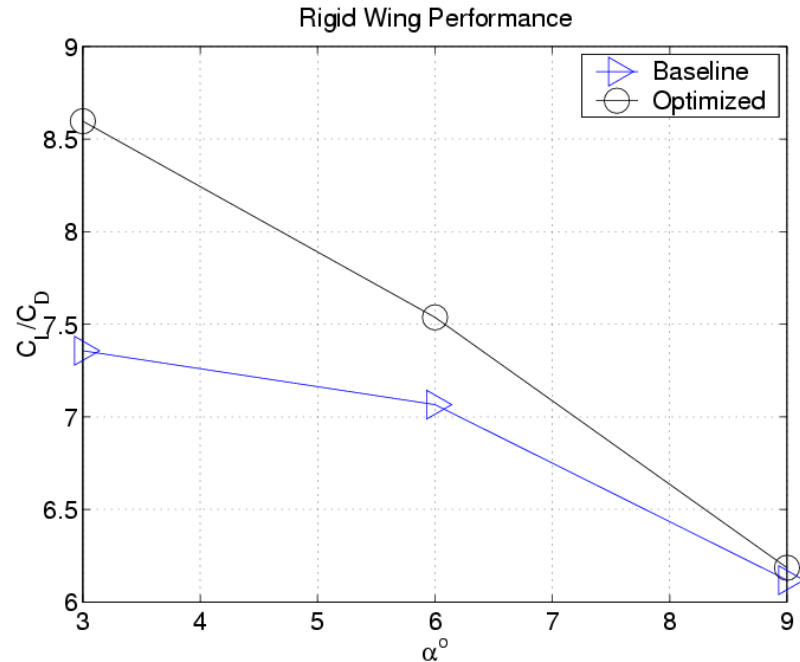
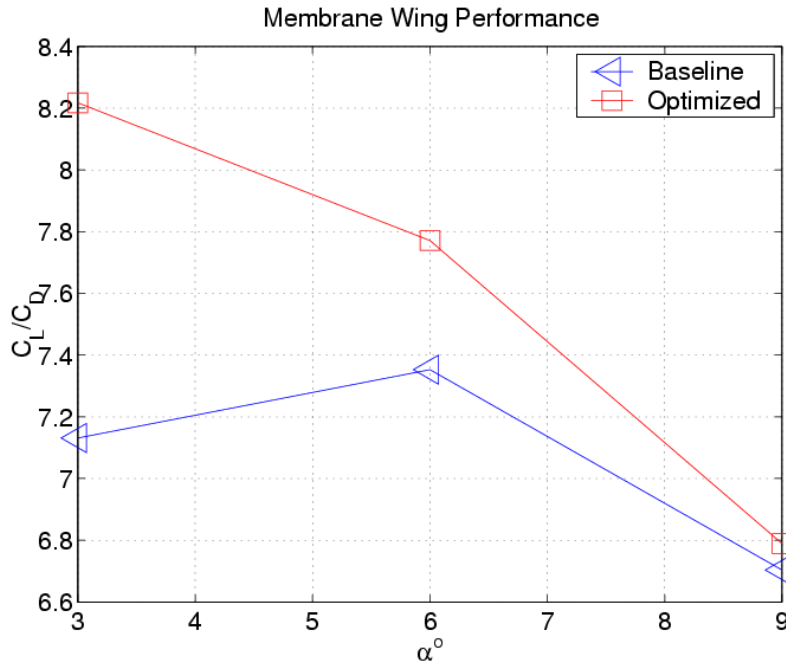
# Spanwise Aerodynamics at Off-Design Point: Rigid Wing at $\text{AoA}=9^\circ$



➤ At large AoA, improvement with the optimized shape diminishes.

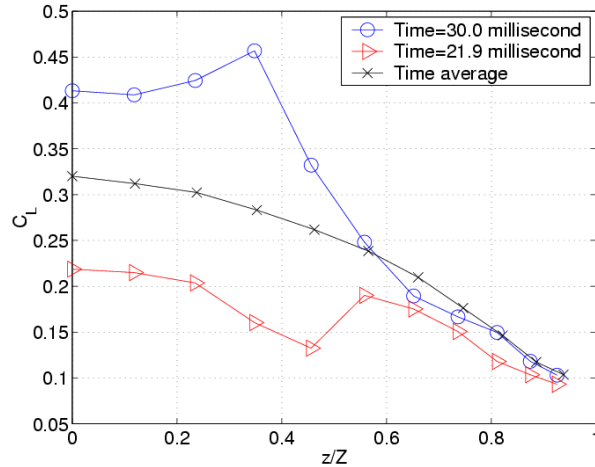


# Aerodynamics Between Membrane & Rigid Wings

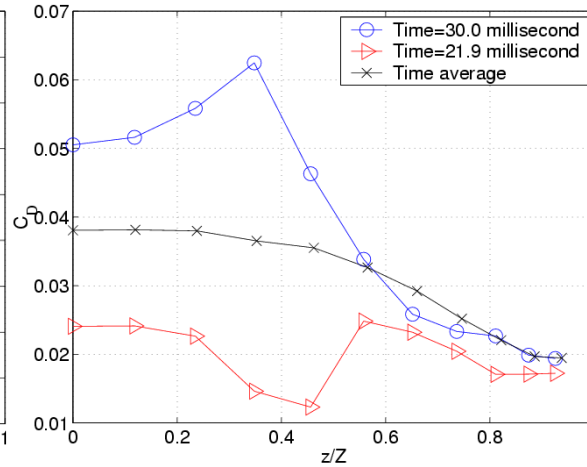


- Optimized shape improves L/D consistently.
- Optimized membrane wing varies less in L/D versus AoA.

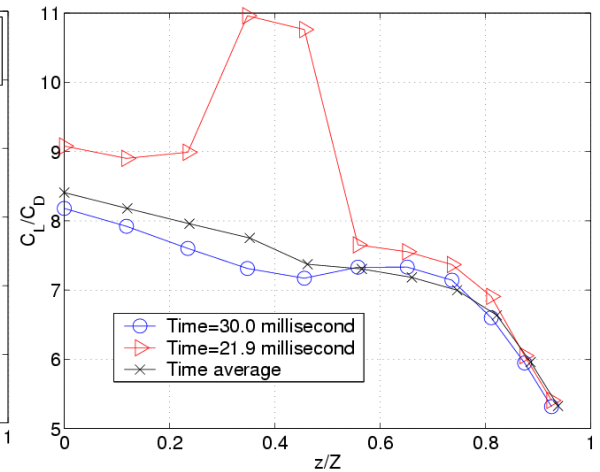
# Optimized Membrane Wing at AoA=6°



Lift



Drag



L/D

➤ While there seem substantial variations in time, the frequency (about 70Hz) is higher than that environmental fluctuation or vehicle response.

# **Outstanding Issues/Opportunities**

- Optimized materials properties for passive flow control.
- Sensor and simplified aerodynamic model to facilitate autonomous flight control.
- Detailed wind tunnel measurements and numerical simulations to assess the unsteady flight environment.
- Efficient propulsion.